

# Oblique Wave Scattering Problems Involving Vertical Porous Membranes

R. Ashok and S. R. Manam

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## Abstract

Oblique surface waves incident on a fixed vertical porous membrane of various geometric configurations is analyzed here. The mixed boundary value problem is modified into easily resolvable problems by using a connection. These problems are reduced to that of solving a couple of integral equations. These integral equations are solved by a one-term or a two-term Galerkin method. The method involves a basis functions consists of simple polynomials multiplied with a suitable weight functions induced by the barrier. Coefficient of reflection and total wave energy are numerically evaluated and analyzed against various wave parameters. Enhanced reflection is found for all the four barrier configurations.

**Keywords** Free surface gravity waves; Reflection coefficient; Singular integral equation; Galerkin approximation; Linear waves; Vertical porous membrane barrier

## 1 Introduction

Free surface water wave scattering problems involving various kind of structures play an important role in science and engineering. Thin vertical barriers are one such structure that attracted lot of attention due to their potential in developing rich mathematical solution methods to the associated boundary value problems. Dean (1945) derived analytical solution of the two-dimensional normally incident water wave problem with a submerged thin vertical rigid barrier by using the complex variable technique. Then, using integral equation procedure, Ursell (1947) studied water wave scattering problem involving a surface piercing rigid barrier. Scattering of gravity waves by a vertical barrier with finite number of gaps in it was discussed by Lewin (1963), Mei (1966) and Evans (1970). Lewin

(1963) and Mei (1966) solved the problem by converting the original problem into a Riemann-Hilbert problem. Evans (1970) used the method of complex variables to obtain the solution of the problem. Mandal and Chakrabarti (2000) proposed various solution methods to obtain the solutions of the wave scattering problems involving different rigid barrier configurations.

Later, porous barriers gained attention due to its reflection and dissipative characteristics. Chwang (1983) introduced porous wave maker theory by involving resistance effects. Then, the condition on the porous barrier has been modified by including inertial effects as well (Yu and Chwang 1994). Further, flexible breakwaters attracted lot more attention due to their structural flexibility. These kind of breakwaters are used in deep sea activities. Incident wave interaction on a flexible barrier that is hinged at the bottom of the sea and moored at the surface was analyzed by Lee and Chen (1990). Also, Williams et al. (1991) investigated flexible floating breakwater that was anchored to the sea floor with a buoy at the free surface.

Kim and Kee (1996) and Cho and Kim (1998) have studied wave interaction with a horizontal tensioned flexible membrane by utilizing the eigenfunction expansion method. Selvan and Behera (2020) have used the same method to handle the effect of a floating circular porous elastic membrane on surface gravity waves. Later, Cho and Kim (2000) discussed interaction of incident waves with a horizontal porous flexible membrane by using the multi-domain boundary element method. Yip et al. (2001)

## Article Highlights

- Vertical flexible porous barrier of four different configuration is handled.
- Galerkin approximation is used to obtain close bounds for the scattering quantities.
- Enhanced reflection and enhanced energy dissipation are found for all barrier configurations.

✉ R. Ashok  
Email: ashokkumaraswin@gmail.com

<sup>1</sup> Department of Mathematics, Indian Institute of Technology Madras, Chennai 600036, India

have investigated the oblique wave scattering problem involving finite number of floating membranes in finite water depth. Then, Suresh Kumar et al. (2007) have analysed wave scattering by a vertical flexible porous membrane in a two-layer fluid of finite depth, using an orthogonality relation along with the least-square approximation. Karmakar and Guedes Soares (2012) have analyzed the performance of the multiple vertical surface-piercing porous membrane barriers in water of finite depth by applying the least-square approximation method. Mandal et al. (2016) studied oblique wave scattering problem involving the multiple flexible porous barriers in a two-layer fluid of finite depth. Using eigenfunction expansion method, Koley and Sahoo (2017) have investigated the oblique wave scattering problem involving different configurations of a vertical flexible porous membrane.

A single term Galerkin's method has been used by Evans and Morris (1972) to handle obliquely incident waves on a surface piercing rigid barrier and they found closed upper and lower bounds for the scattering quantities. Also, scattering of oblique incident surface waves by a finite length thin submerged vertical plate as well as a complete barrier with a gap in it has been handled by Mandal and Das (1996) and Das et al. (2018a, 2019). They used one or two term Galerkin method to find the scattering quantities analytically. Further, Galerkin method with many terms is utilized to solve oblique scattering problem involving a partially immersed and a submerged solid barrier by Das et al. (2018b).

A flexible porous tensioned membrane is considered here with all four type of configurations such as partially immersed, submerged barrier extending infinitely downwards, submerged barrier with a finite length and a complete membrane with a gap in it. Free surface waves incident obliquely on the barrier from either side are considered. This defines two solution velocity potentials for the original problem. The upper-half plane problems for the two velocity potentials are reduced to problems in a quarter-plane. These quarter plane problems are connected with auxiliary potentials through a couple of integral relations. Then, the auxiliary potentials are handled by the Galerkin's method with one or multi-term approximation. Further, lower and upper bounds for the scattering quantities are obtained. Formulation of the boundary value problem and its solution method is described in Section 2. In Section 3, numerical results are discussed for each of the barrier configuration by choosing a suitable weight function in the approximation. Finally, few conclusions are drawn in Section 4.

## 2 Mathematical formulation and method of solution

A mixed boundary value problem is considered in the

Cartesian coordinate system  $(x, y, z)$  with the positive  $y$ -axis is measured vertically downwards and the horizontal  $xz$ -plane is the undisturbed free surface. The fluid is occupied in the domain  $y > 0$  and  $-\infty < x, z < \infty$ . The vertical porous membrane is placed in the fluid region at  $x=0$ ,  $y \in B$  and  $-\infty < z < \infty$  in which  $B$  takes one of the following:  $(0, a)$ ,  $(b, \infty)$ ,  $(0, a) \cup (b, \infty)$  and  $(a, b)$ . The fluid is considered to be inviscid, incompressible and the flow is in irrotational motion. Incident surface waves come from  $x=-\infty$  and make an angle  $\beta$  with the  $xy$ -plane. Under the assumptions of the linearised water wave theory, time-harmonic fluid motion is described by the velocity potential  $\text{Re}\{\phi_1(x, y)e^{ipz}e^{-i\omega t}\}$ , where  $p=K\sin\beta$ ,  $K=\omega^2/g$  in which  $\omega$  is frequency of the incident wave,  $g$  is the acceleration of gravity and  $t$  is time. The same wave motion is also described, when the incident waves come from  $x=\infty$  and make an angle  $\pi-\beta$  with the  $xy$ -plane, by the velocity potential  $\text{Re}\{\phi_2(x, y)e^{ipz}e^{-i\omega t}\}$ . Then, the spacial velocity potentials  $\phi_j(x, y)$ ,  $j=1, 2$  satisfy

$$\frac{\partial^2 \phi_j}{\partial x^2} + \frac{\partial^2 \phi_j}{\partial y^2} - p^2 \phi_j = 0, \quad -\infty < x < \infty, \quad y > 0 \quad (1)$$

The free surface boundary condition is

$$\frac{\partial \phi_j}{\partial y} + K\phi_j = 0 \quad \text{on } y = 0 \quad (2)$$

In addition,  $\phi_j(x, y)$ ,  $j=1, 2$  satisfy the conditions

$$|\nabla \phi_j| \rightarrow 0 \quad \text{as } y \rightarrow \infty \quad (3)$$

and

$$|\nabla \phi_j| \sim r^{-1/2} \quad \text{as } r \rightarrow 0 \quad (4)$$

where  $r$  is the local radius from the edge point of the barrier. The schematic diagram for the oblique wave scattering problem is shown in Figure 1.

The displacement of the horizontally oscillating membrane is represented as

**Figure 1** Free surface with submerged flexible porous membrane

$$\eta_j(y, t) = \text{Re} [v_j(y) e^{(-1)^j i \omega t}], \quad j = 1, 2$$

where  $v_j(y)$  is the deflection amplitude of the membrane.

Assume that the absolute value of the deflection amplitude is small as compared to the incident wave length. The boundary condition on the flexible porous membrane (Yu and Chwang 1994) is given by

$$\frac{\partial \phi_j}{\partial x}(0^\pm, y) = (-1)^j \left[ i\Gamma K (\phi_j(0^+, y) - \phi_j(0^-, y)) - i\omega v_j(y) \right], \quad j = 1, 2, y \in B \quad (5)$$

where  $\Gamma = \Gamma_1 + i\Gamma_2$  is the non-dimensional complex porous effect parameter in which  $\Gamma_1$  is the resistance effect and  $\Gamma_2$  is the inertial effect.

The fluid flow is continuous in the gap  $x=0$ ,  $y \in \bar{B} = (0, \infty) \setminus B$ . That is,

$$\phi_j(0^-, y) = \phi_j(0^+, y), \quad y \in \bar{B}$$

The radiating conditions are described as

$$\phi_j(x, y) \sim \begin{cases} \phi^0(-x, y) + R\phi^0(x, y), & x \rightarrow (-1)^{j+1}\infty, \\ T\phi^0(-x, y), & x \rightarrow (-1)^j\infty, \end{cases} \quad j = 1, 2$$

where  $\phi^0(-x, y) = e^{-iKx \cos\beta - Ky}$  is the incident wave potential and  $R, T$  are amplitudes of the reflected, transmitted waves. Also, the deflection amplitude  $v_j(y)$ ,  $j=1, 2$  of the membrane satisfies the following condition

$$\frac{d^2 v_j}{dy^2} + \alpha^2 v_j = (i\omega\rho/T) [\phi_j(0^+, y) - \phi_j(0^-, y)], \quad j = 1, 2, y \in B$$

In the above,  $T$  is tension in the membrane,  $\rho$  is the density of water. The membrane frequency parameter may be defined as  $\alpha = \omega\sqrt{m_s/T}$ , where  $m_s = \rho_s d_s$  is the uniform mass with  $\rho_s$  and  $d_s$  being the uniform mass density and the thickness of the membrane, respectively.

By utilizing the above equation in Equation (5), the boundary condition on the barrier Equation (5) is obtained as

$$\begin{aligned} & \left[ \frac{\partial^2}{\partial y^2} + \alpha^2 \right] \frac{\partial \phi_j}{\partial x}(0^\pm, y) \\ &= (-1)^j i\Gamma K \left[ \frac{\partial^2 \phi_j(0^+, y)}{\partial y^2} - \frac{\partial^2 \phi_j(0^-, y)}{\partial y^2} \right] \\ &+ (-1)^j (i\Gamma K + \rho/m_s) \alpha^2 [\phi_j(0^+, y) - \phi_j(0^-, y)], \quad j = 1, 2, y \in B \end{aligned} \quad (6)$$

## 2.1 Reduction to quarter-plan problems

In view of the continuity of the horizontal velocity of the fluid across  $x=0$ , the original velocity potentials  $\phi_j$ ,  $j=1, 2$  that are defined in the upper-half plane may be modified into a new potential functions  $\psi_j$ ,  $j=1, 2$  in the quarter-plane. This is done by choosing (Lamb 1932)

$$\begin{aligned} \phi_j(x, y) &= \\ \begin{cases} \phi^0(-x, y) + \phi^0(x, y) + \psi_j(x, y) & \text{if } (-1)^j x < 0 \\ -\psi_j(-x, y) & \text{if } (-1)^j x > 0, \text{ if } j = 1, 2 \end{cases} \end{aligned} \quad (7)$$

The potential functions  $\psi_j$  defined in the domain  $(-1)^{j+1}x > 0$ ,  $j=1, 2$  satisfy Equations (1)–(4). By applying Equation (7) to the Equation (6), the boundary condition on the barrier becomes

$$\begin{aligned} & \left[ \frac{\partial^2}{\partial y^2} + \alpha^2 \right] \frac{\partial \psi_j}{\partial x}(0, y) + 2i\Gamma K \left[ \frac{\partial^2 \psi_j(0, y)}{\partial y^2} + K^2 \phi^0(0, y) \right] \\ &+ 2\alpha^2 (i\Gamma K + \rho/m_s) [\psi_j(0, y) + \phi^0(0, y)] = 0 \text{ if } y \in B, j = 1, 2 \end{aligned} \quad (8)$$

In addition, the boundary condition in the gap and the radiation condition become

$$\psi_j(0, y) + \phi^0(0, y) = 0 \quad \text{for } y \in \bar{B}, j = 1, 2 \quad (9)$$

and

$$\psi_j(x, y) \rightarrow (R-1)\phi^0(x, y) \quad \text{as } (-1)^j x \rightarrow -\infty, \quad j = 1, 2$$

with a note that  $T=1-R$ .

## 2.2 Connection between wave potentials

A well defined connection, similar to the one in Ashok et al. (2020), between the flexible porous wave potential  $\psi_j(x, y)$ ,  $j=1, 2$  and the auxiliary potential  $\chi_j(x, y)$ ,  $j=1, 2$  is introduced as

$$\begin{aligned} & \left[ \frac{\partial^2}{\partial y^2} + \alpha^2 \right] \psi_j(u, y) + i\Gamma K \int_0^x \frac{\partial^2 C_j(u, y)}{\partial y^2} du \\ &+ \alpha^2 (i\Gamma K + \rho/m_s) \int_0^x C_j(u, y) du \\ &= \chi_j(x, y), \quad (-1)^{j+1}x > 0, j = 1, 2 \end{aligned} \quad (10)$$

where  $C_j(u, y) = \phi^0(u, y) + \phi^0(-u, y) + \sum_{m=1}^2 \psi_m((-1)^{j+m}u, y)$ .

The auxiliary potential functions  $\chi_j(x, y)$ ,  $j=1, 2$  satisfy Equations (1)–(4). By differentiating the connection Equation (10), one obtains

$$\left[ \frac{\partial^2}{\partial y^2} + \alpha^2 \right] \psi_{jx}(x, y) + iK\Gamma \frac{\partial^2 C_j(x, y)}{\partial y^2} + \alpha^2 (iK\Gamma + \rho/m_s) C_j(x, y) = \chi_{jx}(x, y), \quad (-1)^{j+1} x > 0, \quad j = 1, 2 \quad (11)$$

where the variable suffix denotes derivative. By setting  $x=0$  in Equation (11) and by applying the equation Equation (8), it may be obtained that

$$\chi_{jx}(0, y) = 0, \quad y \in B, \quad j = 1, 2 \quad (12)$$

Also, by setting  $x=0$  and by using the equation Equation (9) in the connection Equation (10), one finds the condition as given by

$$\chi_j(0, y) = (-\alpha^2 - K^2)\phi^0(0, y), \quad y \in \bar{B}, \quad j = 1, 2 \quad (13)$$

Further, the radiation condition for  $\chi_j(x, y)$ ,  $j=1, 2$  may be specified as

$$\chi_j(x, y) \sim R_j \phi^0(x, y) + T_j \phi^0(-x, y), \quad (-1)^{j+1} x \rightarrow \infty \quad (14)$$

where  $R_j$  and  $T_j$  are constants. By applying the far-field behaviour in each term of the differential form of the connection Equation (11), a pair of relations is obtained as

$$R_1 = T_2 = \left[ (1 + \Gamma)(K^2 + \alpha^2) - \frac{i\alpha^2 \rho}{Km_s} \right] R - \alpha^2 - K^2 \quad (15)$$

and

$$T_1 = R_2 = \left[ -\Gamma(\alpha^2 + K^2) + \frac{i\alpha^2 \rho}{Km_s} \right] R \quad (16)$$

Thus, the problem for the wave potential  $\psi(x, y)$  with  $j=1, 2$  has been decomposed into two solvable auxiliary potential problems with the aid of the connection Equation (10). Hence, the solution of the auxiliary potential  $\psi_j(x, y)$  may be found in terms of the wave potentials  $\chi_j(x, y)$  as in Ashok et al. (2020). The approximate solution of the wave potentials  $\chi_j(x, y)$ ,  $j=1, 2$  is obtained by the Galerkin approximation method which in turn helps to find the estimated value of the reflection coefficient  $|R|$ .

### 2.3 Galerkin method

The general solution of the potential function  $\chi_1(x, y)$  satisfying Equations (1)–(3) and Equation (14) is given by (Manam et al. 2006)

$$\chi_1(x, y) = R_1 \phi^0(x, y) + T_1 \phi^0(-x, y) + \int_0^\infty A(\gamma) B(\gamma, y) e^{\gamma_1 x} d\gamma, \quad x > 0 \quad (17)$$

where  $R_1, T_1$  are unknown constants,  $A(\gamma)$  is an unknown function,  $B(\gamma, y) = \gamma \cos \gamma y - K \sin \gamma y$  and  $\gamma_1 = \sqrt{\gamma^2 + p^2}$ . Let

$$g(y) = \frac{\partial \chi_1}{\partial x}(0, y) \quad \text{and} \quad h(y) = \chi_1(0, y) \quad \text{if } y > 0$$

By utilizing the general solution Equation (17) in the above functions  $g(y)$  and  $h(y)$ , it may be obtained that

$$g(y) = i(R_1 - T_1)K \cos \beta e^{-Ky} - \int_0^\infty \gamma_1 A(\gamma) B(\gamma, y) d\gamma \quad \text{if } y > 0 \quad (18)$$

and

$$h(y) = (R_1 + T_1)e^{-Ky} + \int_0^\infty A(\gamma) B(\gamma, y) d\gamma \quad \text{if } y > 0 \quad (19)$$

Then, the Havelock's inversion theorem (Havelock 1929) is applied to the above pair of equations to get

$$i(R_1 - T_1) \cos \beta = 2 \int_B g(u) e^{-Ku} du \quad (20)$$

$$A(\gamma) = -\frac{2}{\pi} \frac{1}{\gamma_1(\gamma^2 + K^2)} \int_B g(u) B(\gamma, u) du \quad (21)$$

$$(R_1 + T_1) = 2K \int_B h(u) e^{-Ku} du \quad (22)$$

and

$$A(\gamma) = \frac{2}{\pi} \frac{1}{(\gamma^2 + K^2)} \int_B h(u) B(\gamma, u) du \quad (23)$$

By substituting  $A(\gamma)$  from Equations (21) and (23) in the equations Equations (19) and (18) and then using the conditions (12) and (13), it may be obtained that

$$\int_B g(u) C(y, u) du = \frac{\pi}{2} (R_1 + T_1 + \alpha^2 + K^2) e^{-Ky}, \quad y \in \bar{B} \quad (24)$$

and

$$\int_B h(u) D(y, u) du = \frac{\pi}{2} iK \cos \beta (R_1 - T_1) e^{-Ky}, \quad y \in B \quad (25)$$

where

$$C(y, u) = \lim_{\epsilon \rightarrow 0^+} \int_0^\infty \frac{B(\gamma, u) B(\gamma, y)}{\gamma_1(\gamma^2 + K^2)} e^{-\epsilon \gamma} d\gamma$$

and

$$D(y, u) = \lim_{\varepsilon \rightarrow 0^+} \int_0^\infty \frac{\gamma_1 B(\gamma, u) B(\gamma, y)}{\gamma^2 + K^2} e^{-\varepsilon \gamma} d\gamma$$

Now, by defining the functions

$$G(u) = \frac{2g(u)}{\pi(R_1 + T_1 + \alpha^2 + K^2)} \quad \text{and} \\ H(u) = \frac{2h(u)}{i\pi K \cos \beta (R_1 - T_1)}$$

and then, by making use of  $G(u)$  and  $H(u)$  in Equation (24) and Equation (25), one obtains that

$$\int_{\bar{B}} G(u) C(y, u) du = e^{-Ky}, y \in \bar{B} \quad (26)$$

and

$$\int_B H(u) D(y, u) du = e^{-Ky}, y \in B \quad (27)$$

Then, the Equations (20) and (22) are modified as

$$\int_{\bar{B}} G(u) e^{-Ku} du = F \quad (28)$$

and

$$\int_B H(u) e^{-Ku} du = \frac{R_1 + T_1}{\pi^2 K^2 F (R_1 + T_1 + \alpha^2 + K^2)} \quad (29)$$

where

$$F = \frac{i \cos \beta (R_1 - T_1)}{\pi (R_1 + T_1 + \alpha^2 + K^2)}$$

The Equation (15) and Equation (16) are used in the above to find

$$F = \frac{\alpha^2 + K^2 - \left[ (1 + 2\Gamma)(\alpha^2 + K^2) - \frac{2i\alpha^2 \rho}{Km_s} \right] R}{i\pi R \sec \beta (\alpha^2 + K^2)} \quad (30)$$

In a similar manner, the same estimation of the constant  $F$  in terms of the reflection amplitude  $R$  can be obtained for the problem of the auxiliary potential function  $\chi_2(x, y)$ , by the aid of the Equations (15) and (16).

## 2.4 Bounds for $F$

Multi-term Galerkin approximation method is used to find the functions  $G(u)$  and  $H(u)$  in the Equations (26) and (27) (Das et al. 2018b). We first define the symmetric and linear inner products as

$$\langle f, g \rangle = \int_B f(u) g(u) du, \quad \text{and} \quad \langle \langle f, g \rangle \rangle = \int_{\bar{B}} f(u) g(u) du$$

Then, we define a pair of operators  $C$  and  $D$  as

$$(Ch)(y) = \langle \langle C(y, u), h(u) \rangle \rangle \\ \text{and} \quad (Dg)(y) = \langle D(y, u), g(u) \rangle$$

Note that the operators  $C$  and  $D$  are linear, positive semi-definite and self-adjoint. To obtain the function  $G(u)$  in Equation (26), we take the multi-term Galerkin approximation as given by

$$G(y) \approx \sum_{n=0}^N a_n g_n(y), y \in \bar{B} \quad (31)$$

where  $g_n(y)$ ,  $n=0, 1, \dots, N$  may be chosen appropriately for a particular barrier position.

By making use of Equation (31) in Equation (26), and multiplying the function  $g_m(y)$  before integrating over  $\bar{B}$ , we get the linear system of equations

$$\sum_{n=0}^N a_n A_{mn} = G_{m0}, \quad m = 0, 1, \dots, N \quad (32)$$

where

$$A_{mn} = \langle \langle (Cg_n)(y), g_m(y) \rangle \rangle \\ \text{and} \quad G_{m0} = \langle \langle e^{-Ky}, g_m(y) \rangle \rangle$$

The constants  $a_n$ ,  $n=0, 1, \dots, N$  are found by solving the above system of equations. By following Evans and Morris (1972), it is seen that

$$\langle \langle G(y), e^{-Ky} \rangle \rangle \geq \langle \langle \sum_{n=0}^N a_n g_n(y), e^{-Ky} \rangle \rangle$$

By substituting the equation Equation (28) in the above inequality, one obtains that

$$F \geq F_l$$

where

$$F_l = \sum_{n=0}^N a_n G_{n0} \quad (33)$$

Further, the function  $H(u)$  in Equation (27) can be found by considering the multi-term Galerkin approximation

$$H(y) \approx \sum_{n=0}^N b_n h_n(y), \quad y \in B \quad (34)$$

where  $h_n(y)$ ,  $n=0, 1, \dots, N$  is chosen appropriately for a par-

ticular barrier problem. By substituting Equation (34) in Equation (27) and multiplying the function  $h_m(y)$  before integrating over  $B$ , we obtain the linear system of equations for the unknowns  $b_n$ ,  $n=0, 1, \dots, N$  as given by

$$\sum_{n=0}^N b_n B_{mn} = H_{m0}, \quad m = 0, 1, \dots, N$$

where

$$B_{mn} = \langle (Dh_n)(y), h_m(y) \rangle \quad \text{and} \quad H_{m0} = \langle e^{-Ky}, h_m(y) \rangle$$

Again, by following Evans and Morris (1972), it is seen that

$$\langle H(y), e^{-Ky} \rangle \geq \left\langle \sum_{n=0}^N b_n h_n(y), e^{-Ky} \right\rangle$$

By utilizing the Equation (29) in the above inequality, with the use of the far-field Equations (15) and (16), it is obtained that

$$F \leq F_u$$

where

$$F_u = \frac{R - 1}{\pi^2 K^2 R \sum_{n=0}^N b_n H_{n0}} \quad (35)$$

By modifying the relation Equation (30), the reflection coefficient is obtained as

$$R = \frac{(\alpha^2 + K^2)}{i\pi F \sec \beta (\alpha^2 + K^2) + \left[ (1 + 2\Gamma)(\alpha^2 + K^2) - \frac{2i\alpha^2 \rho}{Km_s} \right]}$$

where  $F_l \leq F \leq F_u$ . The upper and lower bounds for the reflection coefficient may now be found as

$$|R_l| \leq |R| \leq |R_u|$$

where

$$R_l = \frac{(\alpha^2 + K^2)}{i\pi F_u \sec \beta (\alpha^2 + K^2) + \left[ (1 + 2\Gamma)(\alpha^2 + K^2) - \frac{2i\alpha^2 \rho}{Km_s} \right]}$$

and

$$R_u = \frac{(\alpha^2 + K^2)}{i\pi F_l \sec \beta (\alpha^2 + K^2) + \left[ (1 + 2\Gamma)(\alpha^2 + K^2) - \frac{2i\alpha^2 \rho}{Km_s} \right]}$$

The upper bound  $R_u$  is computed first and then use it in

the Equation (35) to estimate the lower bound  $F_u$  which is matched with the lower bound  $F_l$ . In the computation, it is found that these bounds for  $F$  are numerically matched up to few decimals.

### 3 Numerical results for various barrier positions

The dimensionless membrane mass and tension parameters  $\delta_1 = \frac{m_s}{\rho l}$  and  $\varepsilon_1 = \frac{T}{\rho g l^2}$  are used in the numerical computation while fixing the value of the length of the porous membrane  $l=2$  m and the density of the sea water  $\rho = 1025$  kg/m<sup>3</sup>. Also, the membrane parameter value  $\alpha = 0.06246$  is obtained by fixing the incident wave frequency  $\omega=1.75$  s<sup>-1</sup>,  $\delta_1=0.01$  and  $\varepsilon_1=0.4$ . Energy identity  $|E|=|R|^2+|T|^2=1$  is verified throughout the computation for the impermeable membrane barrier ( $\Gamma=0$ ). The porous membrane barrier becomes the solid barrier when  $\Gamma=0$  and  $\alpha=0$ . It is seen that the reflection curves are matching with the ones in already published works when  $\Gamma=0$  and  $\alpha=0$  are fixed for all the four barrier configurations.

#### 3.1 Surface piercing finite membrane

In this case, the position and the gap are at  $B=(0,a)$  and  $\bar{B}=(a,\infty)$ , respectively. The function  $G(y)$  has been taken (Das et al. 2018b) as

$$G(y) \approx \frac{e^{-Ky}}{\sqrt{\left(\frac{y}{a}\right)^2 - 1}} \sum_{n=0}^N a_n \left(\frac{y}{a}\right)^n \quad \text{if } y \in (a, \infty)$$

where  $a_n$ ,  $n=0, 1, \dots, N$  are unknown constants and

$$g_n(y) = \frac{e^{-Ky}}{\sqrt{\left(\frac{y}{a}\right)^2 - 1}} \left(\frac{y}{a}\right)^n, \quad y \in (a, \infty), \quad n = 0, 1, \dots, N$$

The nature of the edge behaviour of the membrane is considered for taking the weight function  $g_n(y)$ ,  $n=0, 1, \dots, N$ . Now, we calculate the analytic results for a two-term Galerkin approximation ( $N=1$ ). Consider  $g_0(y)$  and  $g_1(y)$ . Then, by solving the system Equation (32) to obtain  $F_i$  as

$$F_i = a_0 G_{00} + a_1 G_{10}$$

where

$$a_0 = \frac{G_{00}A_{11} - G_{10}A_{01}}{A_{00}A_{11} - A_{01}^2}, \quad a_1 = \frac{G_{00}A_{01} - G_{10}A_{00}}{A_{01}^2 - A_{00}A_{11}}$$

and  $G_{i0}=a K_i(2Ka)$ ,  $i=0, 1$  in which  $K_i(2Ka)$ ,  $i=0, 1$  are modified Bessel functions. It is observed that  $B_{01}=B_{10}$  from symmetry of the kernel of the integral equations. Further,



the constants  $A_{00}$ ,  $A_{01}$  and  $A_{11}$  are known as

$$A_{00} = \int_0^\infty \frac{P^2(\gamma a)}{\gamma_1(\gamma^2 + K^2)} d\gamma, \quad A_{01} = \int_0^\infty \frac{P(\gamma a)Q(\gamma a)}{\gamma_1(\gamma^2 + K^2)} d\gamma$$

and

$$A_{11} = \int_0^\infty \frac{Q^2(\gamma a)}{\gamma_1(\gamma^2 + K^2)} d\gamma$$

where

$$P(\gamma a) = \int_a^\infty \frac{e^{-Ku} B(\gamma, u)}{\sqrt{\left(\frac{u}{a}\right)^2 - 1}} du \quad \text{and}$$

$$Q(\gamma a) = \int_a^\infty \frac{e^{-Ku} B(\gamma, u)}{\sqrt{\left(\frac{u}{a}\right)^2 - 1}} \left(\frac{u}{a}\right) du$$

Also,  $H(y)$  can be taken as

$$H(y) \approx \sqrt{1 - \left(\frac{y}{a}\right)^2} \sum_{n=0}^N b_n \left(\frac{y}{a}\right)^n, \quad \text{if } y \in (0, a)$$

where  $b_n$ ,  $n=0, 1, \dots, N$  are unknown constants. The weight functions  $h_n(y)$ ,  $n=0, 1, \dots, N$  are given by

$$h_n(y) = \left(\frac{y}{a}\right)^n \sqrt{1 - \left(\frac{y}{a}\right)^2} \quad \text{if } y \in (0, a)$$

The same procedure is applied for the two-term Galerkin approximation, as mentioned above, to obtain the upper bound  $F_u$ . It is numerically verified that both the upper and lower bounds are matching up to few decimals to estimate the value of the reflection coefficient  $|R|$ .

The reflection coefficient  $|R|$  and the total energy  $|E| = |R|^2 + |T|^2$  are calculated against the angle of incidence  $\beta$ . In Figures 2 and 3, estimation of the reflection coefficient  $|R|$  and the total energy  $|E|$  are depicted versus the angle of incidence  $\beta$  for various values of the wavenumber  $Ka$  with the membrane frequency parameter  $\alpha=0.06246$  for both

cases of porous as well as impermeable membranes. It may be observed, from Figures 2 and 3, that enhanced reflection and enhanced dissipation occur at smaller incident angles for shorter waves. The angle at which wave reflection gets its resonant peak increases with a decrease in the incident wave number. The reflection peak increases as length of the barrier increases, this is due to larger barrier reflect more waves. Also, complete reflection occurs at these incident angles in the case of the impermeable membrane.

Reflection and energy curves are plotted against the angle of incidence for various values of the membrane frequency parameter  $\alpha$  in Figures 4 and 5. For smaller values of  $\alpha$ , there is neither enhanced reflection nor enhanced energy loss for all angles of wave incidence. Reflection decreases gradually with an increase in the angle of incidence for all values of the membrane frequency parameter. For smaller values of incidence, reflection is higher for the porous membranes with lesser tension. Also, mass of the membrane barrier increases when the reflection increases for shorter waves. This is because of barrier with higher mass reflect better. As expected, energy dissipation is higher for membranes with lower tension at smaller angles of wave incidence. However, enhanced reflection and total wave energy dissipation occur for porous membranes. Reflection or energy dissipation peaks happen at larger incident angles with a decrease in the tension of the porous membrane.

Reflection and energy curves are depicted against the angle of incidence  $\beta$  for different values of the porous effect parameter  $\Gamma$  when the values of  $\alpha=0.06246$  and  $Ka=0.4$  are fixed in Figure 6. It is seen from Figure 6(a) that reflection in general is better for small incident angles when both the resistance and the inertial effects are present in the porous barrier. Further, all the reflection curves have peaks that are due to the flexible nature of the barrier and they occur within  $50^\circ$  to  $75^\circ$ . Also, enhanced reflection is evidently complete for the impermeable membrane. Enhancement of the energy dissipation may be seen from Figure 6(b) around a particular angle of wave incidence for

**Figure 2** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $Ka$  with  $\Gamma=1$  and  $\alpha=0.06246$

**Figure 3** Graph of  $|R|$  versus  $\beta$  for different values of  $Ka$  with  $\Gamma=0$  and  $\alpha=0.06246$

all the values of the porous effect parameter. In Figure 7, reflection and energy curves are plotted against the angle of incidence  $\beta$  for various values of the porous effect parameter  $\Gamma$  when  $\alpha=0$  and  $Ka=0.4$ . Overall reflection significantly decreases again for the resistance as well as the inertial effects for small angles of wave incidence on the porous solid barrier. Figure 7(a) also shows that porosity alone will not cause enhanced reflection by the barrier since there is no evidence of the enhanced reflection in the absence of flexibility in the barrier. Also, as seen from Figure 7(b), en-

ergy dissipation is evidently caused mainly from the inertial effects of the porous barrier. The smaller reflection is noted for the porous membrane barrier due to the fact that the porous barrier allows the water to pass through it.

### 3.2 Submerged membrane of infinite length

The membrane position and gap are at  $B=(b, \infty)$  and  $\bar{B}=(0, b)$  respectively. Again, the multi-term Galerkin approximation is used and  $G(y)$  (Das et al. 2018b) is set as

$$G(y) \approx \frac{1}{\sqrt{1 - (\frac{y}{b})^2}} \sum_{n=0}^N a_n (\frac{y}{b})^n \quad \text{if } y \in (0, b)$$

where  $a_n$ ,  $n=0,1,\dots,N$  are unknowns to be determined and the weight functions  $g_n(y)$ ,  $n=0,1,\dots,N$  are

$$g_n(y) = \frac{1}{\sqrt{1 - (\frac{y}{b})^2}} (\frac{y}{b})^n \quad \text{if } y \in (0, b)$$

Again, the nature of the edge behaviour of the membrane is considered for choosing the weight function  $g_n(y)$ ,  $n=0,1,\dots,N$ . Then, two-term Galerkin approximation ( $N=1$ ) is used to solve the linear system Equations (32). The

**Figure 4** Graph of  $|R|$  and  $|E|$  versus  $\theta$  for different values of  $\alpha$  with  $\Gamma=1$  and  $Ka=0.4$

**Figure 5** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\alpha$  with  $\Gamma=1$  and  $Ka=0.4$



**Figure 6** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\alpha=0.06246$  and  $Ka=0.4$ **Figure 7** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\alpha=0$  and  $Ka=0.4$ 

lower bound  $F_l$  can be obtained as  $F_l = a_0 G_{00} + a_1 G_{10}$ , where

$$a_0 = \frac{G_{00}A_{11} - G_{10}A_{01}}{A_{00}A_{11} - A_{01}^2}, \quad a_1 = \frac{G_{00}A_{01} - G_{10}A_{00}}{A_{01}^2 - A_{00}A_{11}}$$

$$G_{00} = \int_0^b \frac{e^{-Ky}}{\sqrt{1 - (\frac{y}{b})^2}} dy \quad \text{and} \quad G_{10} = \int_0^b \left(\frac{y}{b}\right) \frac{e^{-Ky}}{\sqrt{1 - (\frac{y}{b})^2}} dy$$

In the above, the constants  $A_{00}$ ,  $A_{01}$  and  $A_{11}$  are

$$A_{00} = \int_0^\infty \frac{S^2(\gamma b)}{\gamma_1(\gamma^2 + K^2)} d\gamma, \quad A_{01} = \int_0^\infty \frac{S(\gamma b)T(\gamma b)}{\gamma_1(\gamma^2 + K^2)} d\gamma$$

and

$$A_{11} = \int_0^\infty \frac{T^2(\gamma b)}{\gamma_1(\gamma^2 + K^2)} d\gamma$$

where

$$S(\gamma b) = \int_0^b \frac{B(\gamma, u)}{\sqrt{1 - (\frac{u}{b})^2}} du \quad \text{and} \quad T(\gamma b) = \int_0^b \frac{B(\gamma, u)}{\sqrt{1 - (\frac{u}{b})^2}} \left(\frac{u}{b}\right) du$$

Now,  $H(y)$  can be taken as

$$H(y) \approx e^{-Ky} \sqrt{\left(\frac{y}{b}\right)^2 - 1} \sum_{n=0}^N b_n \left(\frac{y}{b}\right)^n \quad \text{if } y \in (b, \infty)$$

where  $b_n$ ,  $n=0, 1, \dots, N$  are unknown constants. The weight functions  $h_n(y)$ ,  $n=0, 1, \dots, N$  are given by

$$h_n(y) = e^{-Ky} \left(\frac{y}{b}\right)^n \sqrt{\left(\frac{y}{b}\right)^2 - 1} \quad \text{if } y \in (b, \infty)$$

Moreover, the upper bound  $F_u$  is obtained by using the same procedure explained in the two-term Galerkin approximation method.

The reflection coefficient  $|R|$  and the total energy  $|E| = |R|^2 + |T|^2$  are evaluated against the wavenumber  $Kb$  and the angle of incidence  $\beta$  for the submerged barrier extending infinitely downwards.

In Figure 8, numerical estimation of the reflection coefficient  $|R|$  and the total energy  $|E|$  are plotted against the angle of wave incidence  $\beta$  for different values of the wave-number  $Kb$  when  $\Gamma=1$  and  $\alpha=0.06246$ . These curves are also shown in Figure 9 for the non porous membrane with the same flexibility. It is observed from Figure 8 that the reflection and the energy dissipation curves have resonant

**Figure 8** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $Kb$  with  $\Gamma=1$  and  $\alpha=0.06246$

enhancement for all the incident wave numbers. Since the present barrier is the complementary nature of the previous case in the subsection 3.1, the resonant peaks at which enhanced reflection occurs move from lower to higher wave incident angles when the incident waves on the barrier become longer to shorter. This is exactly opposite to the results of the previous complementary case. Similar observation can be made for the energy dissipation curves with the change in the incident wavenumber. Flexibility alone causes the total reflection from the submerged non-porous membrane as seen from Figure 9. Thus, longer waves should incident the membrane by higher oblique angles to get better or complete reflection while shorter waves could incident the membrane by smaller oblique angles for a similar enhanced reflection.

In Figure 10, reflection and energy curves are depicted against the angle of wave incidence for various membrane frequency parameter values when the wavenumber  $Kb=0.4$  and  $\Gamma=1$  are fixed. The reflection peaks move towards higher oblique wave angles as the membrane frequency parameter increases. Similar behaviour is seen in the surface piercing membrane case as well. This shows that only flexibility nature of the barrier, not a type of the barrier, causes the enhanced reflection. The reflection and energy curves are also plotted against the wavenumber for different mem-

**Figure 9** Graph of  $|R|$  versus  $\beta$  for different values of  $Kb$  with  $\Gamma=0$  and  $\alpha=0.06246$

brane frequency parameter values when the angle of oblique incidence  $\beta=30^\circ$  and  $\Gamma=1$  are fixed in Figure 11. However, reflection peaks move towards shorter incident waves as the membrane frequency parameter increases. This suggests longer waves must incident on a high tensioned membrane and shorter waves must incident on a low tensioned membrane to get better resonant reflection. Reflection peak is attained for shorter and moderate waves for smaller mass of the membrane barrier. Similar observations can also be made from the energy curves in Figure 11.

**Figure 10** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\alpha$  with  $\Gamma=1$  and  $Kb=0.4$

**Figure 11** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\alpha$  with  $\Gamma=1$  and  $\beta=30^\circ$

Reflection and energy curves are also depicted against the angle of incidence for various porous effect parameter values when the wavenumber  $Kb=0.4$  and  $\alpha=0.06246$  are fixed in Figure 12. By comparing these curves with the ones in Figure 6, it may be concluded that the reflection and the energy dissipation is mostly caused by the flexible nature of the membrane. Enhanced reflection becomes a complete one for the impermeable barrier at a particular incident wave angle as observed in the case of surface piercing membrane barrier. Figure 13 shows reflection and energy curves for the solid porous barrier. They are qualitative-

ly comparable with the ones in Figure 7.

### 3.3 Submerged membrane of finite length

In this case, the membrane position and the gap are at  $B=(a,b)$  and  $\bar{B}=(0,a)\cup(b,\infty)$  respectively. The Galerkin approximation for  $G(y)$  is specified as  $G(y) \approx \sum_{n=0}^N a_n g_n(y)$ , where  $a_n$ ,  $n=0,1,\dots,N$  are unknown constants and  $g_n(y)$ ,  $n=0,1,\dots,N$  are the weight functions. The nature of the edge conditions of the porous membrane is considered to set  $g_n(y)$  as

**Figure 12** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\alpha=0.06246$  and  $Kb=0.4$

**Figure 13** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\alpha=0$  and  $Kb=0.4$

$$g_n(y) = \begin{cases} \left(\frac{y}{a}\right)^n \sqrt{\frac{a}{a-y}} & \text{if } y \in (0, a) \\ e^{-Ky} \left(\frac{y}{b}\right)^n \sqrt{\frac{b}{y-b}} & \text{if } y \in (b, \infty) \end{cases}$$

Here, we obtain the analytic results by using a single term Galerkin approximation ( $N=0$ ). Consider  $g_0(y)$ . Then, by solving the linear system Equation (32), we obtain  $a_0 = G_{00}/A_{00}$ . By using  $a_0$  into Equation (33) and get  $F_l = G_{00}^2/A_{00}$  where

$$G_{00} = \int_0^a e^{-Ky} \sqrt{\frac{a}{a-y}} dy + \int_b^\infty e^{-2Ky} \sqrt{\frac{b}{y-b}} dy$$

and

$$A_{00} = \int_0^\infty \frac{X^2(\gamma ab)}{\gamma_1(\gamma^2 + K^2)} d\gamma$$

with

$$X(\zeta ab) = \int_0^a B(\gamma, u) \sqrt{\frac{a}{a-u}} du + \int_b^\infty e^{-Ku} B(\zeta, u) \sqrt{\frac{b}{u-b}} du$$

Likewise, a single term Galerkin approximation for the function  $H(y)$  is specified as

$$H(y) \approx \frac{1}{b} \sqrt{(y-a)(b-y)} \sum_{n=0}^N b_n \left(\frac{y}{b}\right)^n \quad \text{if } y \in (a, b)$$

Again, the edge behaviour of the membrane is considered to set  $h_n(y)$ ,  $n=0, 1, \dots, N$  as

$$h_n(y) = \frac{1}{b} \sqrt{(y-a)(b-y)} \left(\frac{y}{b}\right)^n \quad \text{if } y \in (a, b)$$

Then, the upper bound  $F_u$  is obtained by using a single term Galerkin method. Thus, the reflection and the trans-

mission coefficients are attained between two close bounds and the numerical results are obtained for the scattering quantities against various parameters.

The reflection coefficient  $|R|$  and the total energy  $|E| = |R|^2 + |T|^2$  are calculated against the non-dimensional wavenumber  $Kb$  as well as the angle of incidence  $\beta$  for a submerged barrier of finite length. Numerical estimation of the reflection and the energy curves are plotted against the wavenumber  $Kb$  for various  $\mu = \frac{a}{b}$  values when  $\beta = 30^\circ$  and  $\Gamma = 1$  are fixed in Figure 14. For the fixed barrier length parameter  $\mu$ , wave reflection and energy loss reach maximum for waves with a moderate wavelength. The measure of these quantities are remained uniform for moderate to short incident waves. For fixed larger wavenumber, the length of the barrier decreases as reflection decreases. It is due to shorter waves interaction with smaller barriers.

In Figures 15 and 16, the reflection coefficient and the total wave energy are depicted against the wavenumber for different values of the membrane frequency parameter when the oblique angle of incidence  $\beta = 30^\circ$  is fixed, in both cases of the porous and the non-porous membranes, respectively. Reflection increases in general when the tension in the membrane increases for all membrane lengths. Further, enhanced reflection takes place for a specific smaller length of the membrane due to the flexible nature of the barrier. Both reflection and dissipation of wave energy maintain uniformly high for moderate to longer membranes. Similar observations can be made, from Figure 16, in the case of the impermeable tensioned membrane. However, impermeable membranes with higher tension cause significantly higher reflection in comparison with the porous ones.

In Figure 17, the reflection coefficient and the total energy are depicted against the incident wave angle for various  $\Gamma$  values when  $Kb = 0.2$  and  $\alpha = 0.06246$  are fixed. From Figure 17, it may be observed that the enhanced reflection and the enhanced energy loss occur in between  $30^\circ$  to  $50^\circ$  and the curves reach minimum in the vicinity of  $90^\circ$ . Again, this is due to the flexible nature of the submerged membrane. Complete reflection is possible at a specific in-

**Figure 14** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\mu$  with  $\beta = 30^\circ$  and  $\Gamma = 1$

**Figure 15** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\alpha$  with  $\mu=0.05$ ,  $\beta=30^\circ$  and  $\Gamma=1$

$(0, a) \cup (b, \infty)$  and  $\bar{B} = (a, b)$ , respectively. The multi-term Galerkin approximation for the function  $G(y)$  can be taken by

$$G(y) \approx \frac{a}{\sqrt{(y-a)(b-y)}} \sum_{n=0}^N a_n \left(\frac{y}{b}\right)^n \quad \text{if } y \in (a, b)$$

where  $a_n$ ,  $n=0, 1, \dots, N$  are unknown constants. The edge behaviour of the membrane is considered to set the weight functions  $g_n(y)$ ,  $n=0, 1, \dots, N$  as

$$g_n(y) = \frac{a}{\sqrt{(y-a)(b-y)}} \left(\frac{y}{b}\right)^n \quad \text{if } y \in (a, b)$$

**Figure 16** Graph of  $|R|$  versus  $Kb$  for different values of  $\alpha$  with  $\mu=0.05$ ,  $\beta=30^\circ$  and  $\Gamma=0$

cident wave angle for the impermeable tensioned membrane. This resonant reaction from the barrier is absent when one considers solid porous membrane, as shown in Figure 18. Again, reflection and energy curves for the solid membrane are qualitatively similar to the ones in Figures 7 and 13.

### 3.4 Complete membrane with a gap

In this case, the membrane position and the gap are at  $B=$

Likewise, consider  $H(y) \approx \sum_{n=0}^N b_n h_n(y)$ , where  $b_n$ ,  $n=0, 1, \dots, N$  are unknown constants and the edge behaviour of the membrane is considered to choose  $h_n(y)$ ,  $n=0, 1, \dots, N$  as

$$h_n(y) = \begin{cases} \left(\frac{y}{a}\right)^n \sqrt{1 - \left(\frac{y}{a}\right)} & \text{if } y \in (0, a) \\ e^{-Ky} \left(\frac{y}{b}\right)^n \sqrt{\left(\frac{y}{b}\right) - 1} & \text{if } y \in (b, \infty) \end{cases}$$

**Figure 17** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\mu=0.5$ ,  $Kb=0.2$  and  $\alpha=0.06246$

**Figure 18** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\mu=0.5$ ,  $Kb=0.2$  and  $\alpha=0$

The same procedure is used to obtain the bounds for the scattering quantities as given in the previous case and the details are not included here. Graphs of the reflection coefficient and the total energy are depicted by considering parameter values as mentioned in the case of the submerged membrane with a finite length.

In Figure 19, estimated values of the reflection coefficient  $|R|$  and the total energy  $|E|$  are computed against the wavenumber  $Kb$  for different  $\mu=\frac{a}{b}$  values when  $\beta=30^\circ$  and  $\Gamma=1$  are fixed. When a particular frequency of waves incident on the tensioned or the non-tensioned porous membrane with a gap in it, reflection and energy dissipation curves get reso-

nant enhancement for a specific length of the gap.

Graphs of the coefficient of reflection and the total energy are given in Figures 20 and 21 against the wavenumber for various  $\alpha$  values when the porous and the impermeable barrier, respectively, are obliquely incident by waves that make an angle  $\beta=30^\circ$ . They reveal that these curves attain resonant peaks when waves of certain frequency incident on the tensioned membrane barrier with a particular gap length. These peaks move towards higher values of  $Kb$  with a decrease in the tension value of the membrane. It is remarked that resonant reflections become a complete one for the impermeable membrane with a gap.

**Figure 19** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\mu$  with  $\beta=30^\circ$  and  $\Gamma=1$

**Figure 20** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\alpha$  with  $\mu=0.05$ ,  $\beta=30^\circ$  and  $\Gamma=1$



**Figure 21** Graph of  $|R|$  and  $|E|$  versus  $Kb$  for different values of  $\alpha$  with  $\mu=0.05$ ,  $\beta=30^\circ$  and  $\Gamma=0$

Finally, reflection and total energy curves are plotted in Figure 22 against the incident angle for various  $\Gamma$  values when  $\mu=0.5$ ,  $Kb=0.2$  and  $\alpha=0.06246$  are fixed. They reveal that the resonant peaks of these curves are attained at high incident angles as compared to the ones in Figure 17 for the case of the submerged membrane of finite length. Again, enhanced reflection is almost complete when the membrane becomes non-porous. In addition, solid porous barrier will not have any resonant reactions from the incident waves. Also, the reflection and the energy curves in Figure 23 for the solid porous barrier with a gap are comparable qualitatively with those in other barrier configurations.

**Figure 22** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\mu=0.5$ ,  $Kb=0.2$  and  $\alpha=0.06246$

**Figure 23** Graph of  $|R|$  and  $|E|$  versus  $\beta$  for different values of  $\Gamma$  with  $\mu=0.5$ ,  $Kb=0.2$  and  $\alpha=0$

## 4 Conclusions

The present work is concerned with the scattering problem of water waves obliquely incident on four types of the vertical porous membranes such as surface piercing, submerged but finite length, submerged but infinite length and complete one with a finite gap. The original problem is decomposed into a pair of resolvable problems for the auxiliary potentials. These problems are solved by the Galerkin method with a one term or a two term approximation. Closed upper and lower bounds are obtained for the scat-

tering quantities by choosing a suitable weight function in all the four barrier configurations. Then, the graphs of the reflection and the total energy are plotted against various parameters such as the non-dimensional wavenumber and the angle of wave incidence. Enhanced reflection and enhanced energy dissipation are found in all the four barrier configurations and they are sensitive to the incident wave angles as well as the membrane parameters. This is useful in the design of removable breakwaters such as vertical membranes by adjusting the length of the membrane suitably chosen so as to attain maximum reflection in order to

mitigate harmful effects of the incident waves.

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## References

- Ashok R, Gunasundari C, Manam SR (2020) Explicit solutions of the scattering problems involving vertical flexible porous structures. *Journal of Fluids and Structures* 99: 103149. <https://doi.org/10.1016/j.jfluidstructs.2020.103149>
- Cho IH, Kim MH (1998) Interactions of a horizontal flexible membrane with oblique incident waves. *Journal of Fluid Mechanics* 367: 139-161. <https://doi.org/10.1017/S0022112098001499>
- Cho IH, Kim MH (2000) Interactions of horizontal porous flexible membrane with waves. *Journal of Waterway Port Coastal and Ocean Engineering* 126(5): 245-253. [https://doi.org/10.1061/\(ASCE\)0733-950X\(2000\)126:5\(245\)](https://doi.org/10.1061/(ASCE)0733-950X(2000)126:5(245))
- Chwang AT (1983) A porous wave maker theory. *J Fluid Mech* 132: 395-406. <https://doi.org/10.1017/S0022112083001676>
- Das BC, De S, Mandal BN (2018a) The problem of oblique scattering by a thin vertical submerged plate in deep water revisited. *Springer Proceedings in Mathematics and Statistics* 253: 225-236. [https://doi.org/10.1007/978-981-13-2095-8\\_18](https://doi.org/10.1007/978-981-13-2095-8_18)
- Das BC, De S, Mandal BN (2018b) Oblique scattering by thin vertical barriers in deep water : solution by multi-term Galerkin technique using simple polynomials as basis. *J Mar Sci Technol* 23: 915-925. <https://doi.org/10.1007/s00773-017-0520-4>
- Das BC, De S, Mandal BN (2019) Wave propagation through a gap in a thin vertical wall in deep water. *CUBO A Mathematical Journal* 21(3): 93-105. <http://dx.doi.org/10.4067/S0719-06462019000300093>
- Dean WR (1945) On the reflection of surface waves by submerged plane barrier. *Proc Camb Phil Soc* 41: 231-238. <https://doi.org/10.1017/S030500410002260X>
- Evans DV (1970) Diffraction of water waves by a submerged vertical plate. *J Fluid Mech* 40: 433-451. <https://doi.org/10.1017/S0022112070000253>
- Evans DV, Morris CAN (1972) The effect of a fixed vertical barrier on obliquely incident surface waves in deep water. *J Inst Maths Applies* 9: 198-204. <https://doi.org/10.1093/imamat/9.2.198>
- Havelock TH (1929) Forced surface waves on water. *Phil Mag Ser* 8: 569-576. <https://doi.org/10.1080/14786441008564913>
- Karmakar D, Guedes Soares C (2012) Oblique scattering of gravity waves by moored floating membrane with changes in bottom topography. *Ocean Engineering* 54: 87-100. <https://doi.org/10.1016/j.oceaneng.2012.07.005>
- Kim MH, Kee ST (1996) Flexible-membrane wave barrier I: analytic and numerical solutions. *Journal of Waterway Port Coastal and Ocean Engineering* 122(1): 46-53. [https://doi.org/10.1061/\(ASCE\)0733-950X\(1996\)122:1\(46\)](https://doi.org/10.1061/(ASCE)0733-950X(1996)122:1(46))
- Koley S, Sahoo T (2017) Oblique wave trapping by vertical permeable membrane barriers located near a wall. *J Marine Sci Appl* 16: 490-501. <https://doi.org/10.1007/s11804-017-1432-8>
- Lamb H (1932) *Hydrodynamics*. Cambridge University Press, Cambridge
- Lee JF, Chen CJ (1990) Wave interaction with hinged flexible breakwater. *J Hydraulic Res* 28: 283-297. <https://doi.org/10.1080/00221689009499070>
- Lewin M (1963) The effect of vertical barriers on progressive waves. *J Math Phys* 42: 287-300. <https://doi.org/10.1002/sapm1963421287>
- Manam SR, Bhattacharjee J, Sahoo T (2006) Expansion formulae in wave structure interaction problems. *Proceeding of Royal Society London A* 462(2065): 263-287. <https://doi.org/10.1098/rspa.2005.1562>
- Mandal S, Behera H, Sahoo T (2016) Oblique wave interaction with porous flexible barriers in a two-layer fluid. *J Eng Math* 100: 1-31. <https://doi.org/10.1007/s10665-015-9830-x>
- Mandal BN, Chakrabarti A (2000) *WaterWave Scattering by Barriers*. WIT Press, Southampton
- Mandal BN, Das P (1996) Oblique diffraction of surface waves by a submerged vertical plate. *J Engng Math* 30: 459-470. <https://doi.org/10.1007/BF00049246>
- Mei CC (1966) Radiation and scattering of transient gravity waves by vertical plates. *Q J Mech Appl Maths* 19: 417-440. <https://doi.org/10.1093/qjmam/19.4.417>
- Selvan SA, Behera H (2020) Wave energy dissipation by a floating circular flexible porous membrane in single and two-layer fluids. *Ocean Engineering* 206: 107374. <https://doi.org/10.1016/j.oceaneng.2020.107374>
- Suresh Kumar P, Manam SR, Sahoo T (2007) Wave scattering by flexible porous vertical membrane barrier in a two-layer fluid. *Journal of Fluids and Structures* 23(4): 633-647. <https://doi.org/10.1016/j.jfluidstructs.2006.10.011>
- Ursell F (1947) The effect of a fixed vertical barrier on surface waves in deep water. *Proc Camb Phil Soc* 43: 374-382. <https://doi.org/10.1017/S0305004100023604>
- Williams AN, Gaiger PT, McDogal WG (1991) Flexible floating breakwater. *J Waterway Port Coastal Ocean Eng ASCE* 117(5): 429-450. [https://doi.org/10.1061/\(ASCE\)0733-950X\(1991\)117:5\(429\)](https://doi.org/10.1061/(ASCE)0733-950X(1991)117:5(429))
- Yip TL, Sahoo T, Chwang AT (2001) Wave scattering by multiple floating membranes. *The Eleventh International Offshore and Polar Engineering Conference*, 3: 379-384
- Yu X, Chwang AT (1994) Wave induced oscillation in harbor with porous breakwaters. *J Waterway Port Coastal Ocean Eng ASCE* 120(2): 125-144. [https://doi.org/10.1061/\(ASCE\)0733-950X\(1994\)120:2\(125\)](https://doi.org/10.1061/(ASCE)0733-950X(1994)120:2(125))